

Appendix-B

Validation to Cinco-Ley's solution

(Mass-in / Time) – (Mass-out / Time) = (Mass-Accumulation / Time)

$$(q_x \cdot \rho_x) - (q_{x+\Delta x} \cdot \rho_{x+\Delta x}) + 2u (h \cdot \Delta x) \cdot \rho_y = q_{\Delta x} \cdot \rho_{\Delta x}$$

Multiply by Δt :

$$(q_x \cdot \Delta t) + (2u) \cdot (h \cdot \Delta x) \cdot \Delta t - (q_{x+\Delta x} \cdot \Delta t) = q_{\Delta x} \cdot \Delta t$$

$$(q_x \cdot \Delta t) - (q_{x+\Delta x} \cdot \Delta t) = \Delta v$$

Introduce the compressibility equation to MBE:

$$\text{Where: } C = -\frac{1}{v} \frac{\Delta v}{\Delta p} \rightarrow \Delta v = cv \Delta p$$

$$(q_x - q_{x+\Delta x}) \cdot (\Delta t) + (2u) \cdot (h \cdot \Delta x) \cdot \Delta t = cv \Delta p = c \cdot (w_f \cdot h \cdot \Delta x \cdot \varphi) \cdot (p_{t+\Delta t} - p_t)$$

Divide by $(\Delta x \cdot \Delta t)$ and take limit as $\Delta x \rightarrow 0$ & $\Delta t \rightarrow 0$:

$$-\lim_{\Delta x \rightarrow 0} \left(\frac{q_{x+\Delta x} - q_x}{\Delta x} \right) + (2u) \cdot (h) = c \cdot (w_f \cdot h \cdot \varphi) \lim_{\Delta t \rightarrow 0} \left(\frac{p_{t+\Delta t} - p_t}{\Delta t} \right)$$

Equation 1

$$-\frac{dq}{dx} + (2u) \cdot (h) = c \cdot (w_f \cdot h \cdot \varphi) \frac{dp}{dt} \quad (1)$$

Introduce Darcy's law:

$$q = -\frac{k_f A}{\mu} \cdot \frac{dp_f}{dx}, \text{ along fracture}$$

Differentiate both sides w.r.t. x:

$$\frac{d}{dx} \cdot q = -\frac{k_f A}{\mu} \cdot \left(\frac{d}{dx} \cdot \frac{dp_f}{dx} \right)$$

Equation 2

$$\frac{dq}{dx} = -\frac{k_f A}{\mu} \cdot \left(\frac{d^2 p_f}{dx^2} \right) \quad (2)$$

Substitute (39) in (38):

$$\frac{k_f A}{\mu} \cdot \left(\frac{d^2 p_f}{dx^2} \right) + (2u) \cdot (h) = c \cdot (w_f \cdot h \cdot \varphi) \frac{dp_f}{dt}$$

Since, $A = w_f \cdot h$, then:

$$\frac{k_f}{\mu} \cdot w_f \left(\frac{d^2 p_f}{dx^2} \right) + (2u) = c \cdot (w_f \cdot \varphi) \frac{dp_f}{dt}$$

Re-arrange:

Two dimensional diffusivity equations for fluid flowing in fracture plane per unit area

$$\frac{\partial^2 p_f}{\partial x^2} + (2u) \cdot \frac{\mu}{w_f \cdot k_f} = \frac{c\mu\phi}{k_f} \cdot \left(\frac{\partial p_f}{\partial t} \right)$$

Or

Equation 3

$$\frac{\partial^2 p_f}{\partial x^2} + (2u) \cdot \frac{\mu}{w_f \cdot k_f} = 1/\eta_f \cdot \left(\frac{\partial p_f}{\partial t} \right) \quad (3)$$

Now, solve for (u') from Darcy's equation:

Equation 4

$$u' = \frac{q}{A} = -\frac{k}{\mu} \cdot \left. \frac{dp}{dy} \right|_{y \rightarrow 0}, \quad (4)$$

Substitute (41) into equation (40) and re-arrange:

Equation 5

$$\frac{\partial^2 p_f}{\partial x^2} + \frac{2k}{k_f \cdot w_f} \left. \frac{\partial p}{\partial y} \right|_{y=0} = 1/\eta_f \cdot \left(\frac{\partial p_f}{\partial t} \right) \quad (5)$$

Where: $1/\eta_f = C \cdot \frac{c_{tf} \cdot \phi_f \cdot \mu}{k_f}$, $C = 0.000264$

Substituting to dimensionless variables Equation 5, as detailed above, will produce Cinco-Ley's Finite Conductivity Fracture Solution Cinco et al. (1978)) for:

- **Symmetric** system on both sides of the fracture $k_1 = k_2$,
- Accounts for **linear** flow along **y-plane** only:

Equation 6

$$\frac{\partial^2 p_{Df}}{\partial x_D^2} + \frac{2}{(k_f \cdot w_f)_D} \left. \frac{\partial p_D}{\partial y_D} \right|_{y_D=0} = 1/\eta_{fD} \cdot \left(\frac{\partial p_{Df}}{\partial t_{Dxf}} \right) \quad (6)$$

Where: $(k_f w_f)_D = \frac{k_f w_f}{k_r x_f}$

While the FracFault-model assumes:

- **Asymmetric** reservoir $k_1 \neq k_2$,
- Accounts for flow on **x-y plane**:

$$\frac{\partial^2 p_{Df}}{\partial x_D^2} + \frac{1}{F_{CDf}} \left[(k_{D2}) \cdot \left. \frac{\partial p_{D2}}{\partial y_D} \right|_{y_D=0} - (k_{D1}) \cdot \left. \frac{\partial p_{D1}}{\partial y_D} \right|_{y_D=0} \right] = 1/\eta_{Df} \cdot \frac{\partial p_{Df}}{\partial t_{Df}}$$

Where: $(k_f w_f)_D = \frac{k_f w_f}{k_r r_w}$